ACCURATE GAUSSIAN EXPANSION OF STO'S. TEST OF MANY--CENTER SLATER INTEGRALS

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> Received November 16th, 1987 Accepted November 24th, 1987

Dedicated to Dr R. Zahradnik on the occasion of his 60th birthday.

The use of large STO-NG expansions for testing algorithms and procedures designed for the calculation of many-center molecular integrals with Slater basis functions was previously proposed. Expansions up to the STO-12G for the 1s and 2s cases and a method for calculating integrals involving higher quantum numbers were there reported. Here, we present the corresponding expansions from STO-13G to STO-27G. Further tests on the convergence in the integral calculations with the new expansions are also included and the results are compared with those obtained previously. These new expansions are necessary when highly accurate comparisons are required.

In a previous paper¹ we have noted that due to the recent $advances^{2-12}$ towards the solution of the problem of molecular integrals with Slater orbitals (STO's), a procedure for checking the precision of the new computational algorithms becomes desirable. Therefore we have proposed a procedure based on the use of large NG gaussian expansions of the STO's and we have presented the optimized exponents and coefficients up to the 12G ones. A study of the precision reached with these expansions shows us that any NG expansion must be enlarged with three gaussians in order to gain a next correct figure in the evaluation of integrals, so that the 12G expansion cannot ensure, in general, the fifth significant digit. It is clear that larger expansions are necessary for high precision tests.

In this work we present the optimized exponents and coefficients for the expansions from 13G to 27G and we show the improvement in the accuracy of the integrals.

Gaussian Expansions of the Slater Orbitals

As we have previously remarked¹, any unnormalized real STO can be written as a product of a first factor:

$$r^{2E[(n-l-1)/2]}r^l P_l^m(e^{im\phi} \pm e^{-im\phi})/\sqrt{\pm 1}$$

Collection Czechoslovak Chem. Commun. (Vol. 53) (1988)

which is a polynomial of the (x, y, z) cartesian coordinates (with E(x) = Integer part of x) times a second factor which can be, either:

or

$$j = e^{-1}$$
, if $n - l$ is odd

$$f = r e^{-r}$$
, if $n - l$ is even.

In this way, the expansion of arbitrary STO's in terms of the easy-integrable Gaussian-type functions only requires to obtain two NG expansions of the second factor. These two expansions can be written as:

$$f_N = \sum_{i=1}^N c_i \, \mathrm{e}^{-\alpha_i r^2} \,,$$

where both the coefficients and exponents are obtained by minimizing the "distance" $f_N - f$ in the least-squares sense. The iterative procedure used for solving this nonlinear problem was discussed in detail in our previous paper¹. Here we only note that although the numerical problems and the convergence difficulties increase with N, both were solved in a similar way to that employed in our previous paper, i.e. the numerical problems were avoided by working in extended precision and the convergence problems by starting near the minimum. As in the previous study, the selection of the starting point was facilitated by the existence of a clear relation between the exponents corresponding to successive values of N. This relation is illustrated in Tables I and II, where the quotients α_i/α_1 for the larger expansions are collected.* As it can be readily noticed, these quotients tend to form a sequence of "magic numbers", which seems to be the same for both the 1s and 2s expansions, except that, in the second one, a gap arises near the middle of the sequence.

The resulting exponents and coefficients are listed in Tables III and IV. We stress that they correspond to the screening constant ζ equal to 1 and that those corresponding to any arbitrary screening constant ζ can be obtained, as usual¹³ by the relation $\alpha_i \leftarrow \zeta^2 \alpha_i$.

Accuracy in the Calculation of Many-Center Slater Integrals

We have employed these new expansions for analyzing the convergence in the calculation of many-center integrals. The calculations were performed with the aid of a computer program developed in our laboratory on the basis of the formulas and algorithm described by V. R. Saunders¹⁴. For comparative purposes, we have chosen the same

^{*} It should be noted that squared roots of the quotients $\sqrt{(\alpha_i/\alpha_1)}$, are given in Table I of ref.¹, while the Tables I and II of the present article contain the quotients α_i/α_1 .

TABLE I					
Relation between the α -parameters of the STO-NG expansions of STO-1s:					
(Each column collects the quotient a_i/a_1 in increasing order of the i-index)					
22	22	24	25	26	27
0.10000F + 01	$0.10000F \pm 01$	$0.10000F \pm 0.1$	$0.10000E \pm 01$	$0.10000E \pm 01$	$0.10000F \pm 01$
$0.18344E \pm 00$	$0.18344E \pm 00$	0.18344F + 00	$0.18344F \pm 00$	0.18344F + 00	0.18344F + 00
0.51383E - 01	0.51383E - 01	0.51383E - 01	0.51383E - 01	0.51383E - 01	0.51383E - 01
0.17708E-01	0.17708E-01	0.17708E - 01	0.17708E-01	0.17708E-01	0.17708E-01
0.69483E-02	0.69483E-02	0.69483E-02	0.69483E - 02	0.69483E-02	0.69483E - 02
0.29867E-02	0.29867E-02	0.29867E-02	0.29867E-02	0.29867E-02	0.29867E-02
0.13751E - 02	0.13751E-02	0.13751E-02	0.13751E - 02	0.13751E-02	0.13751E-02
0.66830E - 03	0.66830E - 03	0.66831E - 03	0.66831E - 03	0.66831E - 03	0.66831E - 03
0.33945E - 03	0.33945E - 03	0.33945E - 03	0.33945E - 03	0.33945E - 03	0.33945E - 03
0.17888E - 03	0.17889E - 03	0.17889E - 03	0.17889E - 03	0.17889E - 03	0.17889E - 03
0.97275E - 04	0.97278E - 04	0.97280E - 04	0.97281E-04	0.97282E - 04	0.97283E - 04
0.54353E - 04	0.54355E = 04	0.5435/E = 04	0.54358E - 04	0.54359E - 04	0.54359E - 04
0.31100E - 04	0.31103E = 04	0.31104E = 04	0.31100E - 04	0.31106E - 04	0.3110/E = 04
0.18174E = 04 0.10821E = 04	0.18170E = 04 0.10873E = 04	0.18178E = 04 0.10825E = 04	0.13179E = 04 0.10826E = 04	0.16179E = 04 0.10827E = 04	0.18180E = 04 0.10827E = 04
0.103212 - 04	0.10823E = 04 0.65547E - 05	0.10823E = 0.4	0.10820E = 04 0.65575E - 05	0.10827E = 04	0.10827E = 04
0.40267E - 05	0.00347E = 05 0.40303E = 05	0.00004E = 0000000000000000000000000000000	0.00075E = 00000000000000000000000000000000000	0.00382E = 05 0.40341E - 05	0.000000 = 0000000000000000000000000000
0.25074E - 05	0.25120E - 05	0.25143E - 05	0.25156E - 05	0.25164E - 05	0.25169E - 05
0.15782E-05	0.15844E-05	0.15874E-05	0.15890E - 05	0.15899E - 05	0.15904E - 05
0.10002E - 05	0.10090E-05	0.10131E - 05	0.10151E-05	0.10162E-05	0.10168E-05
0.63299E - 06	0.64631E-06	0.65219E-06	0.65497E - 06	0.65636E-06	0.65710E-06
0.39050E - 06	0.41308E - 06	0.42195E - 06	0.42591E-06	0.42780E-06	0.42876E-06
	0.25719E-06	0.27217E-06	0.27812E - 06	0.28081E - 06	0.28211E - 06
1		0.17092E - 06	0.18094E - 06	0.18496E - 06	0.18680E - 06
			0.11455E - 06	0.12130E - 06	0.12405E - 06
				0.77380E-07	U.81966E - 07
					0.52664E - 07
L					

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TABLE II						
Relation between the α -parameters of the STO-NG expansions of STO-2s:						
(Each column collects the quotient α_i/α_1 in increasing order of the i-index)						
22	23	24	25	26	27	
0.10000E + 01	0.10000E + 01	0.10000E + 01	0.10000E + 01	0.10000E + 01	0.10000E + 01	
0.18344E + 00	0.18344E + 00	0.18344E + 00	0.18344E + 00	0.18344E + 00	0.18344E + 00	
0.51382E - 01	0.51383E – 01	0.51383E - 01	0.51383E – 01	0.51383E – 01	0.51383E – 01	
0.17708E - 01	0.17708E - 01	0.17708E - 01	0.17708E-01	0.17708E-01	0.17708E - 01	
0.69483E – 02	0.69483E - 02	0.69483E – 02	0.69483E-02	0.69483E – 02	0.69483E – 02	
0.29867E - 02	0.29867E - 02	0.29867E - 02	0.29867E - 02	0.29867E - 02	0.29867E - 02	
0.13750E - 02	0.13750E - 02	0.13751E - 02	0.13751E - 02	0.13751E - 02	0.13751E - 02	
0.66826E - 03	0.66825E - 03	0.66830E - 03	0.66830E - 03	0.66830E - 03	0.66831E - 03	
0.33940E - 03	0.33938E - 03	0.33945E - 03	0.33945E – 03	0.33945E-03	0.33945E – 03	
0.17883E - 03	0.17879E - 03	0.17890E - 03	0.17889E - 03	0.17889E - 03	0.17889E – 03	
0.97212E - 04	0.97139E - 04	0.97305E - 04	0.97288E - 04	0.97281E - 04	0.97277E - 04	
0.54279E - 04	0.54175E - 04	0.54399E - 04	0.54372E - 04	0.54359E - 04	0.54353E - 04	
0.31021E - 04	0.30886E - 04	0.31168E - 04	0.31127E - 04	0.31108E - 04	0.31098E - 04	
0.18097E - 04	0.17937E - 04	0.18265E - 04	0.18211E - 04	0.18184E - 04	0.18169E - 04	
0.10760E - 04	0.10584E - 04	0.10936E - 04	0.10870E - 04	0.10834E - 04	0.10815E - 04	
	0.63384E - 05	0.66885E - 05	0.66125E - 05	0.65691E - 05	0.65442E - 05	
0.40182E - 05	•	· · · · · · · · · · · · · · · · · · ·	0.40979E – 05	0.40488E - 05	0.40192E - 05	
0.25233E - 05	0.23808E - 05	0.26643E - 05		0.25350E - 05	0.25021E - 05	
0.16117E - 05	0.14960E - 05	0.17326E - 05	0.16615E - 05		0.15779E – 05	
0.10447E - 05	0.95559E - 06	0.11467E - 05	0.10853E - 05	0.10401E - 05	-	
0.68424E - 06	0.61927E - 06	0.77025E - 06	0.71986E – 06	0.68109E - 06	0.65207E - 06	
0.44881E - 06	0.40545E - 06	0.52337E - 06	0.48375E - 06	0.45213E - 06	0.42749E - 06	
0.28786E - 06	0.26585E - 06	0.35797E – 06	0.32845E - 06	0.30380E - 06	0.28387E - 06	
	0.17045E – 06	0.24432E - 06	0.22433E - 06	0.20613E - 06	0.19071E - 06	
1		0.16265E – 06	0.15283E - 06	0.14066E - 06	0.12935E - 06	
			0.10154E - 06	0.95728E - 07	0.88217E - 07	
				0.63532E - 07	0.60008E - 07	
					0.39805E – 07	

TABLE III					
a- and c-parameters	for the STO-NG expans	ions of the STO-1S with	exponent equal to		
•	one. $(\hat{N} = 1)$	3 to 16).	• •		
STO-13G a	$e^{a} = 6.9(-11)$	STO-14G E ^a =	= 2.1(-11)		
$\boldsymbol{\alpha}_{i}$	c _i	α_i	c _i		
0 1215407025E + 04	0 1633603621E - 01	$0.2145377075E \pm 04$	0 12703236888 01		
0.1313407023E + 04	0.10330730212 = 01 0.2583660675E - 01	0.2145577075E + 03	0.1277523000E 01		
0.2412303020E + 03	0.3933224310F - 01	0.1102331133E + 03	0.2023003727E 01		
$0.07329165930F \pm 02$	0.5736417056F - 01	0.3798874530F + 02	0.4510326502E - 01		
$0.9138581942E \pm 01$	0.8038476703E - 01	$0.1490547441E \pm 02$	0.6360888319E - 01		
0.3927673620E + 01	$0.1078177598E \pm 00$	0.6406579555E + 01	0.8651685053E - 01		
$0.1807837198E \pm 01$	0.1364781739E + 00	0.2949148146E + 01	0.1127068119E+00		
0.8781872806E+00	0.1582344586E+00	0.1432914928E+01	0.1382448991E+00		
0.4455908687E+00	0.1590215202E + 00	0.7274236354E+00	0.1545029374E+00		
0.2342633181E+00	0.1258397926E+00	0.3829153388E+00	0.1484819790E+00		
0.1266267248E+00	0.6653386136E-01	0.2076926940E+00	0.1112352941E+00		
0.6959022430E-01	0.1756699004E - 01	0.1153107605E + 00	0.5508142042E-01		
0.3779259742E-01	0.1246786212E - 02	0.6485370488E - 01	0.1349273683E-01		
		0.3594217442E - 01	0.8819637529E-03		
STO 150					
S (O- 15G)	**********	′ STO-16G ε° =	= 7 7(-17)		
\$10-15G 8	$E^{*} = 6.6(-12)$	STO-16G ε* =	= 2.2(-12)		
α _i	c ⁻ = 6.6(-12) c _i	α _i	= 2.2(-12) c _i		
α_i 0.3446098165E + 04	$c_i = 6.6(-12)$ $c_i = 0.1009455830E - 01$	α_{i} 0.5459188399E + 04	= 2.2(-12) c _i 0.8020447259E ~ 02		
α_i 0.3446098165E + 04 0.6321504192E + 03	$c_i = 6.6(-12)$ $c_i = 0.1009455830E - 010.1597262916E - 01$	α_{i} 0.5459188399E + 04 0.1001431818E + 04	^c i 0.8020447259E ~ 02 0.1269225302E - 01		
α_i 0.3446098165E + 04 0.6321504192E + 03 0.1770674923E + 03	c_i c_i 0.1009455830E - 01 0.1597262916E - 01 0.2435557149E - 01	α_{i} 0.5459188399E + 04 0.1001431818E + 04 0.2805052207E + 03	^c i 0.8020447259E - 02 0.1269225302E - 01 0.1936074073E - 01		
α_i 0.3446098165E + 04 0.6321504192E + 03 0.1770674923E + 03 0.6102187492E + 02	c_i c_i 0.1009455830E - 01 0.1597262916E - 01 0.2435557149E - 01 0.3567518010E - 01	α_{i} 0.5459188399E + 04 0.1001431818E + 04 0.2805052207E + 03 0.9666961441E + 02	c_{i} 0.8020447259E - 02 0.1269225302E - 01 0.1936074073E - 01 0.2838682758E - 01		
α_i 0.3446098165E + 04 0.6321504192E + 03 0.1770674923E + 03 0.6102187492E + 02 0.2394328741E + 02	c_i 0.1009455830E - 01 0.1597262916E - 01 0.2435557149E - 01 0.3567518010E - 01 0.5050531108E - 01	α_i 0.5459188399E + 04 0.1001431818E + 04 0.2805052207E + 03 0.9666961441E + 02 0.3793085880E + 02	c _i 0.8020447259E - 02 0.1269225302E - 01 0.1936074073E - 01 0.2838682758E - 01 0.4028079449E - 01		
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α_{i} 0.3446098165E + 04 0.6321504192E + 03 0.1770674923E + 03 0.6102187492E + 02 0.2394328741E + 02 0.1029148520E + 02 0.4737775054E + 01	c_{i} c_{i} $0.1009455830E - 01$ $0.1597262916E - 01$ $0.2435557149E - 01$ $0.3567518010E - 01$ $0.5050531108E - 01$ $0.6927061680E - 01$ $0.9180422181E - 01$	α_i 0.5459188399E + 04 0.1001431818E + 04 0.2805052207E + 03 0.9666961441E + 02 0.3793085880E + 02 0.1630404012E + 02 0.7505970039E + 01	c_i 0.8020447259E - 02 0.1269225302E - 01 0.1936074073E - 01 0.2838682758E - 01 0.4028079449E - 01 0.5552867417E - 01 0.7436539192E - 01		
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α_i 0.3446098165E + 04 0.6321504192E + 03 0.1770674923E + 03 0.6102187492E + 02 0.2394328741E + 02 0.1029148520E + 02 0.4737775054E + 01 0.2302229857E + 01 0.1169015323E + 01 0.6157054066E + 00 0.3344122161E + 00 0.1863432414E + 00 0.1059100137E + 00 0.007020466E + 01 0.007020466E + 01 0.33441221661E + 00 0.33441221661E + 00 0.1863432414E + 00 0.007020466E + 01 0.007020466E + 01 0.007020466E + 01 0.33441221661E + 00 0.007020466E + 01 0.33441221661E + 00 0.007020466E + 01 0.007020466E + 01 0.007020466E + 01 0.33441221661E + 00 0.007020466E + 01 0.007020466E + 01 0.007020466E + 01 0.007020466E + 02 0.00702046E + 02 0.00702040E + 02 0.0070204E + 02 0.00702	c_{i} c_{i} 0.1009455830E - 01 0.1597262916E - 01 0.2435557149E - 01 0.3567518010E - 01 0.5050531108E - 01 0.6927061680E - 01 0.9180422181E - 01 0.1164650474E + 00 0.1386988872E + 00 0.1496829642E + 00 0.1378369694E + 00 0.9801977489E - 01 0.4562509752E - 01 0.4562509752E - 01	α_i 0.5459188399E + 04 0.1001431818E + 04 0.2805052207E + 03 0.9666961441E + 02 0.3793085880E + 02 0.1630404012E + 02 0.7505970039E + 01 0.3647617627E + 01 0.3647617627E + 01 0.9758920644E + 00 0.5303572460E + 00 0.2959603789E + 00 0.1688575914E + 00 0.90140927E + 01 0.9014092E + 01 0.90140020E + 01 0.901400	c_{i} 0.8020447259E - 02 0.1269225302E - 01 0.136074073E - 01 0.2838682758E - 01 0.4028079449E - 01 0.5552867417E - 01 0.7436539192E - 01 0.9629531104E - 01 0.1191965574E + 00 0.1380320581E + 00 0.1440546701E + 00 0.1273348360E + 00 0.8616339385E - 01		
α_i 0.3446098165E + 04 0.6321504192E + 03 0.1770674923E + 03 0.1770674923E + 02 0.2394328741E + 02 0.1029148520E + 02 0.4737775054E + 01 0.2302229857E + 01 0.1169015323E + 01 0.6157054066E + 00 0.3344122161E + 00 0.1863432414E + 00 0.1059100137E + 00 0.6079710651E - 01 0.41001400E 01 0.41004400E 01 0.4100440E 01 0.410440E 01 0.410440E 01 0.410440E 01 0.410440E	c_i c_i 0.1009455830E - 01 0.1597262916E - 01 0.2435557149E - 01 0.3567518010E - 01 0.505531108E - 01 0.6927061680E - 01 0.9180422181E - 01 0.1164650474E + 00 0.1386988872E + 00 0.13869684E + 00 0.1378369694E + 00 0.91977489E - 01 0.4562509752E - 01 0.1041658728E - 01	α_i 0.5459188399E + 04 0.1001431818E + 04 0.2805052207E + 03 0.9666961441E + 02 0.3793085880E + 02 0.1630404012E + 02 0.7505970039E + 01 0.3647617627E + 01 0.1852402951E + 01 0.9758920644E + 00 0.5303572460E + 00 0.2959603789E + 00 0.1688575914E + 00 0.9798149837E - 01 0.67391464837E - 01	c_i 0.8020447259E - 02 0.1269225302E - 01 0.1936074073E - 01 0.2838682758E - 01 0.4028079449E - 01 0.4028079449E - 01 0.7436539192E - 01 0.7436539192E - 01 0.9629531104E - 01 0.1191965574E + 00 0.1380320581E + 00 0.1440546701E + 00 0.1273348360E + 00 0.3782278426E - 01 0.3782278426E - 01		
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α_i 0.3446098165E + 04 0.6321504192E + 03 0.1770674923E + 03 0.1770674923E + 02 0.2394328741E + 02 0.1029148520E + 02 0.4737775054E + 01 0.230229857E + 01 0.1169015323E + 01 0.6157054066E + 00 0.3344122161E + 00 0.1863432414E + 00 0.1059100137E + 00 0.6079710651E - 01 0.3431061600E - 01	c_{i} 0.1009455830E - 01 0.1597262916E - 01 0.2435557149E - 01 0.3567518010E - 01 0.5050531108E - 01 0.6927061680E - 01 0.9180422181E - 01 0.1166650474E + 00 0.1386988872E + 00 0.1378369894E + 00 0.137836994E + 00 0.9801977489E - 01 0.4562509752E - 01 0.1041658728E - 01 0.6302861489E - 03	$\begin{array}{c} \alpha_i \\ 0.5459188399E + 04 \\ 0.1001431818E + 04 \\ 0.2805052207E + 03 \\ 0.9666961441E + 02 \\ 0.3793085880E + 02 \\ 0.1630404012E + 02 \\ 0.7505970039E + 01 \\ 0.3647617627E + 01 \\ 0.3647617627E + 01 \\ 0.9758920644E + 00 \\ 0.5303572460E + 00 \\ 0.2959603789E + 00 \\ 0.3285938681E - 01 \\ 0.3285938681E - 01 \\ \end{array}$	c_i 0.8020447259E - 02 0.1269225302E - 01 0.1936074073E - 01 0.2838682758E - 01 0.4028079449E - 01 0.5552867417E - 01 0.7436539192E - 01 0.7436539192E - 01 0.7436539192E - 01 0.191965574E + 00 0.180320581E + 00 0.1440546701E + 00 0.1273348360E + 00 0.1273348360E + 00 0.8616339385E - 01 0.3782278426E - 01 0.8080736456E - 02 0.4546331359E - 03		

α - and c-parameter	TABLE II s for the STO-NG expans one. (N=1	II (cont.) sions of the STO-1S with 17 to 20).	exponent equal to	
STO-17G $\varepsilon^{a} = 7.3(-13)$		STO-18G $\varepsilon^{a} = 2.5(-13)$		
α_i	c _i	$\boldsymbol{\alpha}_{i}$	c _i	
$\begin{array}{l} 0.8539172306\mathrm{E}+04\\ 0.1566424260\mathrm{E}+04\\ 0.4387626762\mathrm{E}+03\\ 0.1512098732\mathrm{E}+03\\ 0.5933153450\mathrm{E}+02\\ 0.2550311352\mathrm{E}+02\\ 0.1174123991\mathrm{E}+02\\ 0.5706016136\mathrm{E}+01\\ 0.2897941908\mathrm{E}+01\\ 0.1526915784\mathrm{E}+01\\ 0.8300511623\mathrm{E}+00\\ 0.2648565311\mathrm{E}+00\\ 0.2648565311\mathrm{E}+00\\ 0.1543028324\mathrm{E}+00\\ 0.9120776095\mathrm{E}-01\\ 0.5420474587\mathrm{E}-01\\ 0.3155866745\mathrm{E}-01\\ \end{array}$	$\begin{array}{c} 0.6413008737E-02\\ 0.1014923909E-01\\ 0.1548518309E-01\\ 0.2271825177E-01\\ 0.3228344506E-01\\ 0.4464388924E-01\\ 0.6017537819E-01\\ 0.6017537819E-01\\ 0.7891316760E-01\\ 0.1210015151E+00\\ 0.1364191426E+00\\ 0.1378531151E+00\\ 0.1378531151E+00\\ 0.137853151E+00\\ 0.137853155E-01\\ 0.3138607933E-01\\ 0.6297418650E-02\\ 0.3307382803E-03\\ \end{array}$	$\begin{array}{c} 0.1320178595E+05\\ 0.2421734400E+04\\ 0.6783396976E+03\\ 0.2337752896E+03\\ 0.9172880745E+02\\ 0.3942906888E+02\\ 0.1815277124E+02\\ 0.8822100536E+01\\ 0.4480707497E+01\\ 0.2361048474E+01\\ 0.1283684989E+01\\ 0.7170255073E+00\\ 0.4100116368E+00\\ 0.2392633185E+00\\ 0.1420186437E+00\\ 0.8535567641E-01\\ 0.5148728804E-01\\ 0.303499049E-01\\ 0.303499049E-01\\ \end{array}$	$\begin{array}{c} 0.5157720645E-02\\ 0.8162988751E-02\\ 0.1245645368E-01\\ 0.1828176158E-01\\ 0.2600240414E-01\\ 0.3602871860E-01\\ 0.3602871860E-01\\ 0.6445134741E-01\\ 0.6445134741E-01\\ 0.639546701E-01\\ 0.1030850663E+00\\ 0.1340179783E+00\\ 0.1340179783E+00\\ 0.1340179783E+00\\ 0.1074117308E+00\\ 0.6622659323E-01\\ 0.2607438909E-01\\ 0.492895972E-02\\ 0.2429502873E-03\\ \end{array}$	
STO-19G	$\varepsilon^{a} = 8.9(-14)$	STO-20G ε ^a	= 3.2(-14)	
α_{i}	c_{i}	α_i	c _i	
$\begin{array}{l} 0.2019129024E+05\\ 0.3703889506E+04\\ 0.1037478315E+04\\ 0.3575452123E+03\\ 0.1402940314E+03\\ 0.6030481075E+02\\ 0.2776399296E+02\\ 0.1349327060E+02\\ 0.6853346968E+01\\ 0.3611439362E+01\\ 0.36173492E+01\\ 0.1963673492E+01\\ \end{array}$	$\begin{array}{c} 0.4170565421E-02\\ 0.6600834265E-02\\ 0.1007357400E-01\\ 0.1478808191E-01\\ 0.2104528803E-01\\ 0.2919651839E-01\\ 0.3961459898E-01\\ 0.5262695440E-01\\ 0.6836432098E-01\\ 0.6836432098E-01\\ 0.8645470922E-01\\ 0.1054813612E+00\\ \end{array}$	$\begin{array}{l} 0.3057377073E+05\\ 0.5608452381E+04\\ 0.1570956734E+04\\ 0.5413978511E+03\\ 0.2124346963E+03\\ 0.9131444574E+02\\ 0.4204087246E+02\\ 0.2043200443E+02\\ 0.1037775161E+02\\ 0.5468807545E+01\\ 0.2973735292E+01\\ \end{array}$	$\begin{array}{c} 0.3389255245E-02\\ 0.5364338691E-02\\ 0.8187028460E-02\\ 0.1202047655E-01\\ 0.1711289568E-01\\ 0.2376001022E-01\\ 0.3229121736E-01\\ 0.4303646818E-01\\ 0.5624657578E-01\\ 0.7192311571E-01\\ 0.8949389001E-01\\ \end{array}$	

0.9505256082E+00

0.5552868397E+00

0.3304336002E + 00

0.1998230323E+00

0.1224684076E+00

0.7575825322E-01

0.4690146243E-01

0.2834749861E-01

0.1217896175E+00

0.1274014187E+00

0.1175916816E + 00

0.8953504394E-01

0.5066721317E-01

0.1806363869E-01

0.3056325630E-02

0.1331751259E-03

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*Squared error in the norm of the expansion.

0.6275075151E+00

0.3664534072E + 00

0.2178937418E+00

0.1315256733E+00

0.8025036185E-01

0.4906875960E-01

0.2931965334E-01

0.1309700827E+00

0.1244762813E + 00

0.9819060624E-01

0.5795181774E-01

0.2168836357E-01

0.3873738157E-02

0.1791033810E-03

TABLE III (cont.) α - and c-parameters for the STO-NG expansions of the STO-1S with exponent equal to one. (N = 21 to 24).					
STO-21G ε	STO-21G $\varepsilon^{a} = 1.2(-14)$		= 4.5(-15)		
$\boldsymbol{\alpha}_{i}$	C,	α_{i}	\mathbf{c}_{i}		
$\begin{array}{l} 0.4586552246E+05\\ 0.8413572280E+04\\ 0.2356686072E+04\\ 0.8121837107E+03\\ 0.3186864862E+03\\ 0.1369867333E+03\\ 0.6306845709E+02\\ 0.3065166014E+02\\ 0.3065166014E+02\\ 0.8204410653E+01\\ 0.4461384929E+01\\ 0.4461384929E+01\\ 0.1426244965E+01\\ 0.3024833490E+00\\ 0.3960874818E+00\\ 0.3002488344E+00\\ 0.3002488344E+00\\ 0.1145778341E+00\\ 0.717553011E-01\\ 0.2494734279E-01\\ 0.2745613911E-01\\ \end{array}$	$\begin{array}{l} 0.2767175967E-02\\ 0.4379796101E-02\\ 0.6684677252E-02\\ 0.9815656419E-02\\ 0.1397732692E-01\\ 0.1941655541E-01\\ 0.2641634136E-01\\ 0.2641634136E-01\\ 0.3528028794E-01\\ 0.3528028794E-01\\ 0.5962049161E-01\\ 0.7513747900E-01\\ 0.7513747900E-01\\ 0.9207656424E-01\\ 0.1085159614E+00\\ 0.1207956360E+00\\ 0.1234232933E+00\\ 0.1107240618E+00\\ 0.8146607752E-01\\ 0.4427022162E-01\\ 0.542035024E-02\\ 0.964961123E-04\\ \end{array}$	$0.68209^{1}3712E + 05$ 0.1251228636E + 05 0.3504758174E + 04 0.1207843738E + 04 0.4739367865E + 03 0.2037210100E + 03 0.2037210100E + 02 0.4558415680E + 02 0.2315332565E + 02 0.1220154594E + 02 0.6635063999E + 01 0.73707350911E + 01 0.2121323005E + 01 0.7380730562E + 00 0.4468871447E + 00 0.2746578538E + 00 0.1710287576E + 00 0.1076471838E + 00 0.6822044693E - 01 0.4317573097E - 01	$\begin{array}{c} 0.2269130318E-02\\ 0.3591533825E-02\\ 0.5481725447E-02\\ 0.8049792527E-02\\ 0.1146454685E-01\\ 0.1593133907E-01\\ 0.2168981239E-01\\ 0.2900744278E-01\\ 0.2900744278E-01\\ 0.4937843550E-01\\ 0.4937843550E-01\\ 0.6275154581E-01\\ 0.7801783597E-01\\ 0.9422657980E-01\\ 0.19327379E+00\\ 0.119333640E+00\\ 0.119333640E+00\\ 0.139557962E+00\\ 0.7398664287E-01\\ 0.3866374389E-01\\ 0.3866374389E-01\\ 0.1258140016E-01\\ 0.1923495104E-02\\ \end{array}$		
STO-23G ε	a =1.7(-15)	0.2663534456E – 01 STO-24G ε ^a =	0.7500422729E - 04 = 6.9(-16)		
$\boldsymbol{\alpha}_{i}$	c_{i}	$\boldsymbol{\alpha}_{\mathrm{i}}$	c,		
$\begin{array}{l} 0.1006133757E+06\\ 0.1845652193E+05\\ 0.5169770882E+04\\ 0.1781656978E+04\\ 0.6990913934E+03\\ 0.3005036235E+03\\ 0.3005036235E+03\\ 0.1383518590E+03\\ 0.6724028435E+02\\ 0.3415315612E+02\\ 0.9787477642E+01\\ 0.5468873619E+01\\ 0.3129359396E+01\\ 0.1628761831E+01\\ 0.6594911115E+00\\ 0.4054988578E+00\\ 0.2527374992E+00\\ 0.1594071849E+00\\ 0.1594071849E+00\\ 0.6502773634E-01\\ 0.4156159945E-01\\ 0.2587657724E-01\\ \end{array}$	$\begin{array}{l} 0.1868329033E-02\\ 0.2957168952E-02\\ 0.4513574089E-02\\ 0.6628371272E-02\\ 0.9441122057E-02\\ 0.9441122057E-02\\ 0.1312249449E-01\\ 0.1787393828E-01\\ 0.2392581481E-01\\ 0.3152810329E-01\\ 0.4092481417E-01\\ 0.5229631975E-01\\ 0.6564333648E-01\\ 0.8057526109E-01\\ 0.9596801419E-01\\ 0.1095136691E+00\\ 0.1146166867E+00\\ 0.1146166867E+00\\ 0.9735064211E-01\\ 0.6708647291E-01\\ 0.375765019E-01\\ 0.375765019E-01\\ 0.375765019E-01\\ 0.375788553E-02\\ 0.5676698346E-04\\ \end{array}$	$\begin{array}{l} 0.1472781066E+06\\ 0.2701670309E+05\\ 0.7567524176E+04\\ 0.2607994568E+04\\ 0.102332282E+04\\ 0.4398784340E+03\\ 0.2025202140E+03\\ 0.9842686389E+02\\ 0.4999380353E+02\\ 0.2634649139E+02\\ 0.1432720668E+02\\ 0.1432720668E+02\\ 0.8005604855E+01\\ 0.4581005748E+01\\ 0.2677182449E+01\\ 0.1594291353E+01\\ 0.9656205117E+00\\ 0.5938595532E+00\\ 0.3703067216E+00\\ 0.2337884595E+00\\ 0.1492052517E+00\\ 0.9605340487E-01\\ 0.6214459394E-01\\ 0.6214459394E-01\\ 0.4008427519E-01\\ 0.2517262997E-01\\ \end{array}$	$\begin{array}{c} 0.1544231705E-02\\ 0.2444200014E-02\\ 0.3730662211E-02\\ 0.5478791159E-02\\ 0.7804251644E-02\\ 0.7804251644E-02\\ 0.1084898255E-01\\ 0.1478177138E-01\\ 0.1979862189E-01\\ 0.2611921184E-01\\ 0.3397427960E-01\\ 0.3397427960E-01\\ 0.4357461539E-01\\ 0.4357461539E-01\\ 0.5504539891E-01\\ 0.6830020661E-01\\ 0.8282148151E-01\\ 0.9732510294E-01\\ 0.1093586932E+00\\ 0.1150924384E+00\\ 0.1099466758E+00\\ 0.9995658360E-01\\ 0.6074584243E-01\\ 0.2946943207E-01\\ 0.8811754859E-02\\ 0.1226965595E-02\\ 0.4318765729E-04\\ \end{array}$		
^a Squared error in the	norm of the expansion.				

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α- a	ind c-parameters for the 9	TABLE STO-NG expansions of t	III (cont.) he STO-1S with exponen		.o 27).
STO-25G E	a = 2.7(-16)	STO-26G ^{£¹}	¹ = 1.1(-16)	STO-27G E ^a	'= 4.6(-17)
α	c.	ă	ن ت	α _i	Ű
0.2140365093E+06	0.1280966755E-02	0.3089405512E + 06	0.1066214253E - 02	0.4430575248E+06	0.8903320126E-03
0.3926286867E + 05	0.2027510660E - 02	0.5667207210E + 05	0.1687603650E - 02	0.8127449816E + 05 0 2276542763E + 05	0.1409218801E 02 0.2150970473E 02
0.3790150266E+04	0.4544883914E - 02	0.5470708062E + 04	0.3783014416E - 02	0.7845647220E + 04	0.3159012588E - 02
0.1487190177E + 04	0.6474247653E-02	0.2146612622E+04	0.5389122555E-02	0.3078498564E+04	0.4500291766E - 02
0.6392675550E + 03	0.900099534E 02	0.9227200164E+03	0.7492885510E - 02	0.1323290798E + 04	0.6257371205E - 02 0 8529463503E - 02
0.1430422752E+03	0.1643625010E - 01	0.2064677428E + 03	0.1368804426E - 01	0.2960996655E+03	0.1143424029E - 01
0.7265537703E+02	0.2170001644E-01	0.1048711711E+03	0.1808105907E-01	0.1503980495E + 03	0.1510927002E-01
0.3828915019E+02	0.2826548180E-01	0.5526688724E+02	0.2357387503E-01	0.7925957106E+02	0.1971201559E - 01
0.2082172409E+02	0.3634251431E - 01	0.3005435862E + 02	0.3036115370E - 01	0.4310177902E + 02	0.2541650437E - 01
0.1105405921E + U2 0.6657719770F + 01	0.5767607061F - 01	0.10/9308940E ± 02 0.9609981873E ± 01	0.3805007378E - 01	0.1378207306E + 02	0.4083566275E - 01
0.3890919796E+01	0.7072667457E - 01	0.5616369279E + 01	0.6003979656E - 01	0.8054745015E + 01	0.5081400538E - 01
0.2317172254E+01	0.8476828636E - 01	0.3344814247E+01	0.7292837476E - 01	0.4797056469E + 01	0.6228815632E-01
0.1403543061E+01	0.9832166336E - 01	0.2026080997E + 01	0.8642846632E - 01	0.2905832400E + 01	0.7491100344E - 01
0.8632881011E + 00	0.1088230565E + 00	0.1246284811E + 01	0.9898183275E - 01	0.1787514132E + 01	0.8781470838E - 01
0.5384384197E + 00	0.1124976381E+00	0.7774164518E + 00 0.4011700044E + 00	0.10/9460889E+00	0.1115111393E + 01 0 7046770506E + 00	0.9932906463E 01 0 1067640414E +- 00
0.2172752700E+00	0.8480938539E - 01	0.3139473758E + 00	0.1003901333E + 00	0.4505011410E + 00	0.1065956832E + 00
0.1401877273E + 00	0.5493958216E - 01	0.2027772255E+00	0.7893299409E - 01	0.2911317884E + 00	0.9560218008E - 01
0.9116064440E - 01	0.2572507876E - 01	0.1321658262E + 00	0.4963737552E - 01	0.1899640621E + 00	0.7334335007E - 01
0.5952831221E - 01	0.7389969470E - 02	0.8675337613E-01	0.2245748270E - 01	$0.1249889240E \pm 00$	0.4480/503/4E - 01
0.38/26//142E - 01	0.98455/8224E - 03 0.3301888770E - 04	0.5/14315202E - 01 0.3777455461E - 01	0.620615//21E-02 0.7073631307E-03	0.82/6409041E - 01 0 5405076167E - 01	0.1960/433/3E - 01 0.5210158234F - 02
10 71/41/4/1047.0	L0 7(1)00010CC'0	0.2390588682E - 01	0.2536148168E - 04	0.3631553319E - 01	0.6394872001E - 03
				0.2333337459E - 01	0.1956566625E - 04
^a Squared error in the nor	m of the expansion.				
	· · · · · · · · · · · · · · · · · · ·				

TABLE IV					
a- and c-parameters	s for the STO-NG expansi	ons of the STO-2S with	exponent equal to		
	one. $(N = 1)$	3 to 16).			
STO 120	að 0 0/ 11)	STO 140 al	- 1.5(11)		
S10-13G	$e^{-2} = 2.3(-11)$	S10-14G E ⁻	= 1.5(-11)		
α _i	c _i	α _i	c _i		
0 1459054940E + 04	0 15507458218 - 01	0 1200260025E ± 04	0 15924429298 - 01		
0.14367346400 ± 04 0.2676246061E \pm 03	-0.1330743821E = 01 0.2448985649E = 01	$0.1399200933E \pm 04$ 0.2566751010E \pm 03	-0.1383443828E = 01		
0.2070240901E + 03	-0.24489890492 = 01	0.23007310102 + 03 0.7189394191E + 02	-0.2300307733E = 01		
0.74939442242 + 02 0.2583091497E + 02	-0.57715715852 = 01	0.777748639E + 02	-0.5452076166E - 01		
$0.1013424026E \pm 02$	-0.7276670166E 01	0.24777480552 + 02 0.9726114746E + 01	-0.7395819807E - 01		
0.4355827977F + 01	-0.9117266576E - 01	0.4188287307F + 01	-0.9192424136F - 01		
$0.2006308261E \pm 01$	-0.9841862791E - 01	0.1939499385E + 01	-0.9745444059E - 01		
$0.9774261007E \pm 00$	-0.7488080784F - 01	$0.9564053226F \pm 00$	-0.7178020653E - 01		
$0.2674098619E \pm 00$	$0.1127032201E \pm 00$	$0.2760286501E \pm 00$	$0.1001724733E \pm 00$		
$0.1488262284E \pm 00$	$0.1827601110E \pm 00$	$0.1598935537E \pm 00$	0.1648608000E + 00		
0.8556849963E - 01	0.1359699658E+00	0.9635304316E - 01	$0.1393003881E \pm 00$		
0.5019852073E - 01	0.4110053091E - 01	0.5978722240E - 01	0.6055116363E - 01		
0.2918689431E-01	0.2894951563E - 02	0.3767840549E-01	0.1079181794E - 01		
		0.2344691416E - 01	0.4405566813E - 03		
STO-15G	$\varepsilon^{*} = 3.2(-12)$	STO-16G c*:	= 7.7(-13)		
α _i	c _i	α _i	c _i		
-					
0.2668209957E+04	-0.1146968696E - 01	0.4963957387E+04	-0.8410143140E - 02		
0.4894508695E + 03	-0.18131832/6E - 01	0.910582/194E + 03	-0.133027748E = 01		
0.13/0949/25E + 03	-0.2/56/443/4E - 01	$0.2550558165E \pm 03$	-0.2026226361E - 01		
0.4724031938E+02	-0.4006384048E - 01	0.8/89820409E + 02	-0.29392/1999E - 01		
$0.1634018343E \pm 02$	-0.5300104433E = 01	$0.3448900903E \pm 02$	-0.4100003418E = 01		
$0.7973083233E \pm 01$ 0.3678341011E \pm 01	-0.7314033313E = 01	$0.1482080380E \pm 02$ 0.6820816770E ± 01	-0.30100/1023E = 01		
$0.3078341011E \pm 01$	-0.8820002932E = 01	$0.0829810779E \pm 01$	-0.7191809400E = 01		
0.17979172312 + 01 0.9253704044E \pm 00	0.6570321021E = 01	0.33230723442 ± 01	-0.8470838408E = 01		
$0.9233704044E \pm 00$	-0.037332132115 01 0.0248006322E - 01	0.1090021912E + 01 0.9030554321E + 00	-0.6132388931E - 01		
0.2827050000E + 00	$0.1582065207E \pm 00$	0.903033432112 ± 00 $0.2871382315E \pm 00$	0.8784817452E = 01		
$0.1011367211E \pm 00$	0.1382003207E + 00 0.1430372115E + 00	$0.1703207165E \pm 00$	0.1548228482F + 00		
0.6294077200E - 01	0.6856781070E - 01	$0.1037800816E \pm 00$	0.1455253122F + 00		
0.3959583435E-01	0.1386893312E - 01	0.6450118171E - 01	0.7289389238E-01		
0.2450262902E - 01	0.6610815897E - 03	0.4044410509E - 01	0.1543713263E - 01		
		0.2492063724E-01	0.7711338058E-03		
^a Squared error in the	e norm of the expansion.				

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TABLE IV (cont.)					
α- and c-parameter	s for the STO-NG expans	ions of the STO-2S with	exponent equal to		
-	one. $(N = 1)$	7 to 20).			
STO-17G $\varepsilon^{a} = 2.5(-13)$		STO-18G $\varepsilon^{a} = 1.3(-13)$			
α_{i}	\mathbf{c}_{i}	α_{i}	c _i		
0.01000010070 + 04	0 (31194(000) 03	0.165701010677 + 05	0 4(000)((000)) 00		
$0.9100231387E \pm 04$	-0.0211840090E - 02	$0.165/919196E \pm 0.04$	-0.4602366399E - 02		
0.1009340908E + 04	-0.9626362969E - 02	$0.3041281008E \pm 04$	-0.7283203380E - 02		
0.40738708935 ± 03	-0.1498486919E - 01	0.8318/31/828+03	-0.1110988362E - 01		
$0.1011421813E \pm 03$	-0.219412139912-01	$0.2933779400E \pm 03$	-0.1028982553E - 01		
$0.0322709933E \pm 02$	-0.3103443034E = 01	0.1151909831E+03	-0.2311703458E - 01		
0.1251182280E + 02	-0.424/819233E = 01	$0.4930974208E \pm 02$	-0.318/43/3//E - 01		
$0.1231182289E \pm 02$	-0.3003019480E - 01	0.2278764707E+02	-0.4270893940E - 01		
$0.0080912304E \pm 01$	-0.7033024244E = 01	$0.1100032213E \pm 02$	-0.5555450823E - 01		
$0.3089471238E \pm 01$	-0.8130101330E - 01	0.3010330874E±01	-0.0854/4/042E = 01		
$0.1029844303E \pm 01$	-0.81/092//02E - 01	$0.29452224/3E \pm 01$	-0.7888127977E - 01		
$0.8889300427E \pm 00$	-0.38332293978-01	0.1391177352E+01	-0.7900904881E = 01		
0.2893380802E + 00	0.8552057552E=01	0.8813700673E+00	-0.300/1//233E - 01		
0.1723074639E + 00	$0.1334008923E \pm 00$	$0.2906392712E \pm 00$	0.845241905/E = 01		
0.1030104439E + 00	$0.14083488/4E \pm 00$	$0.1/31347/29E \pm 00$	$0.1328724049E \pm 00$		
0.6518333710E - 01	0.7486814604E - 01	$0.1055110399E \pm 00$	$0.14/4005282E \pm 00$		
0.4079720475E = 01	0.10128/9304E - 01	0.6545199004E - 01	0.7500185548E = 01		
0.2308814423E = 01	0.8192/32999E - 03	0.40933238918-01	0.1040100009E - 01		
		0.2515170344E - 01	0.8381/39093E - 03		
STO-19G	$c^{a} = 4.5(-1.4)$	STO-28C ca	- 1 2(14)		
	c = 4.0(-1 4)	310-200 6	- 1.2(-14)		
	2 - 4.5(-14)	310-203 8	- 1.2(-14)		
α,	c _i	α _i	- 1.2(-14) c _i		
α,	¢ _i	α _i	- 1.2(-14) c _i		
α _i 0.1541972558E+05	c _i -0.4772248864E - 02	α _i 0.2657973404E+05	c_i -0.3634920018E - 02		
α_i 0.1541972558E + 05 0.2828589380E + 04	-0.4772248864E - 02 -0.7551926479E - 02	α_i 0.2657973404E + 05 0.4875781996E + 04	- 1.2(-14) c _i -0.3634920018E - 02 -0.5752657548E - 02		
α_i 0.1541972558E + 05 0.2828589380E + 04 0.7922996438E + 03	c_i -0.4772248864E - 02 -0.7551926479E - 02 -0.1151923151E - 01	α_i 0.2657973404E + 05 0.4875781996E + 04 0.1365729337E + 04	$\begin{array}{c} c_{i} \\ -0.3634920018E - 02 \\ -0.5752657548E - 02 \\ -0.8777233728E - 02 \\ \end{array}$		
α_i 0.1541972558E + 05 0.2828589380E + 04 0.7922996438E + 03 0.2730479755E + 03	c_i -0.4772248864E - 02 -0.7551926479E - 02 -0.1151923151E - 01 -0.1688770930E - 01	α_i 0.2657973404E + 05 0.4875781996E + 04 0.1365729337E + 04 0.4706688272E + 03	$\begin{array}{c} c_{i} \\ -0.3634920018E - 02 \\ -0.5752657548E - 02 \\ -0.8777233728E - 02 \\ -0.1287752504E - 01 \end{array}$		
α_i 0.1541972558E + 05 0.2828589380E + 04 0.7922996438E + 03 0.2730479755E + 03 0.1071382784E + 03 0.1071382784E + 03	c_{i} -0.4772248864E - 02 -0.7551926479E - 02 -0.1151923151E - 01 -0.1688770930E - 01 -0.2395701308E - 01	α_i 0.2657973404E + 05 0.4875781996E + 04 0.1365729337E + 04 0.4706688272E + 03 0.1846809908E + 03	$\begin{array}{c} c_{i} \\ -0.3634920018E - 02 \\ -0.5752657548E - 02 \\ -0.8777233728E - 02 \\ -0.1287752504E - 01 \\ -0.1830094211E - 01 \\ -0.1830094211E - 01 \end{array}$		
α_i 0.1541972558E + 05 0.2828589380E + 04 0.7922996438E + 03 0.2730479755E + 03 0.1071382784E + 03 0.4605330333E + 02	c_{i} -0.4772248864E - 02 -0.7551926479E - 02 -0.1151923151E - 01 -0.1688770930E - 01 -0.2395701308E - 01 -0.3300383374E - 01	α_i 0.2657973404E + 05 0.4875781996E + 04 0.1365729337E + 04 0.4706688272E + 03 0.1846809908E + 03 0.7938436608E + 02 0.7938436608E + 02	$\begin{array}{c} c_{i} \\ -0.3634920018E - 02 \\ -0.5752657548E - 02 \\ -0.8777233728E - 02 \\ -0.1287752504E - 01 \\ -0.1830094211E - 01 \\ -0.2531192708E - 01 \\ -0.2531182708E - 01 \\ -0.25781828020000000000000000$		
α_i 0.1541972558E + 05 0.2828589380E + 04 0.7922996438E + 03 0.2730479755E + 03 0.1071382784E + 03 0.4605330333E + 02 0.2120425083E + 02 0.2120425083E + 02	c_i -0.4772248864E - 02 -0.7551926479E - 02 -0.1151923151E - 01 -0.1688770930E - 01 -0.2395701308E - 01 -0.3300383374E - 01 -0.4412923411E - 01 -0.620276722 01	α_i 0.2657973404E + 05 0.4875781996E + 04 0.1365729337E + 04 0.4706688272E + 03 0.1846809908E + 03 0.7938436608E + 02 0.3654888101E + 02 0.3654888101E + 02	$\begin{array}{c} c_{i} \\ -0.3634920018E - 02 \\ -0.5752657548E - 02 \\ -0.8777233728E - 02 \\ -0.1287752504E - 01 \\ -0.1830094211E - 01 \\ -0.2531192708E - 01 \\ -0.3412641398E - 01 \\ -0.341264126414841888 \\ -0.34126418484848484848484848484848484848484848$		
α_i 0.1541972558E + 05 0.2828589380E + 04 0.7922996438E + 03 0.2730479755E + 03 0.1071382784E + 03 0.4605330333E + 02 0.2120425083E + 02 0.1030836509E + 02 0.62020001E + 01	c_i -0.4772248864E - 02 -0.7551926479E - 02 -0.1151923151E - 01 -0.1688770930E - 01 -0.2395701308E - 01 -0.3300383374E - 01 -0.4412923411E - 01 -0.5692007677E - 01	α_i 0.2657973404E + 05 0.4875781996E + 04 0.1365729337E + 04 0.4706688272E + 03 0.1846809908E + 03 0.7938436608E + 02 0.3654888101E + 02 0.1776447645E + 02	$\begin{array}{c} c_i\\ -0.3634920018E-02\\ -0.5752657548E-02\\ -0.8777233728E-02\\ -0.1287752504E-01\\ -0.1830094211E-01\\ -0.2531192708E-01\\ -0.3412641398E-01\\ -0.4476266061E-01\\ -0.4476266061E-01\\ -0.6476260061E-01\\ -0.6476260061E-01\\ -0.66720089000\\ -0.66720089000\\ -0.66720089000\\ -0.6672008900\\ -0.6672008900\\ -0.6672008900\\ -0.6672008900\\ -0.6672008900\\ -0.6672008900\\ -0.6672008900\\ -0.667200890\\ -0.667200890\\ -0.667200890\\ -0.667200890\\ -0.667200890\\ -0.667200890\\ -0.667200890\\ -0.667200890\\ -0.667200890\\ -0.667200890\\ -0.667200890\\ -0.667200890\\ -0.66720080\\ -0.6720080\\ -0.$		
α_i 0.1541972558E + 05 0.2828589380E + 04 0.7922996438E + 03 0.2730479755E + 03 0.1071382784E + 03 0.4605330333E + 02 0.2120425083E + 02 0.2120425083E + 02 0.2240720981E + 01 0.27604040E + 01	c_i -0.4772248864E - 02 -0.7551926479E - 02 -0.1151923151E - 01 -0.1688770930E - 01 -0.2395701308E - 01 -0.3300383374E - 01 -0.4412923411E - 01 -0.5692007677E - 01 -0.6976617596E - 01	α_i 0.2657973404E + 05 0.4875781996E + 04 0.1365729337E + 04 0.4706688272E + 03 0.1846809908E + 03 0.7938436608E + 02 0.3654888101E + 02 0.1776447645E + 02 0.9025753924E + 01	$\begin{array}{c} c_{i} \\ -0.3634920018E - 02 \\ -0.5752657548E - 02 \\ -0.8777233728E - 02 \\ -0.1287752504E - 01 \\ -0.1830094211E - 01 \\ -0.2531192708E - 01 \\ -0.3412641398E - 01 \\ -0.4476266061E - 01 \\ -0.5671998830E \\ -0.567198840E \\ -0.5671998840E \\ -0.567198840E \\ -0.567198840E \\ -0.56719840E \\ -0.5671840E \\$		
α_i 0.1541972558E + 05 0.2828589380E + 04 0.7922996438E + 03 0.2730479755E + 03 0.400530332E + 02 0.2120425083E + 02 0.1030836509E + 02 0.5240720981E + 01 0.2768741245E + 01 0.2168444202E + 01	c_{i} -0.4772248864E - 02 -0.7551926479E - 02 -0.1151923151E - 01 -0.1688770930E - 01 -0.2395701308E - 01 -0.3300383374E - 01 -0.4412923411E - 01 -0.5692007677E - 01 -0.6976617596E - 01 -0.7872832352E - 01 -0.7872632352E - 01	α_i 0.2657973404E + 05 0.4875781996E + 04 0.1365729337E + 04 0.4706688272E + 03 0.1846809908E + 03 0.7938436608E + 02 0.3654888101E + 02 0.1776447645E + 02 0.9025753924E + 01 0.4760750694E + 01 0.4760750694E + 01	$\begin{array}{c} c_{i} \\ -0.3634920018E - 02 \\ -0.5752657548E - 02 \\ -0.8777233728E - 02 \\ -0.1287752504E - 01 \\ -0.1830094211E - 01 \\ -0.2531192708E - 01 \\ -0.3412641398E - 01 \\ -0.4476266061E - 01 \\ -0.6836367592E - 01 \\ -0.5671998830E - 01 \\ -0.6836367592E - 01 \\ -0.6836367592E - 01 \\ -0.5671998830E - 01 \\ -0.5671998800E \\ -0.567199800$		
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α_i 0.1541972558E + 05 0.2828589380E + 04 0.7922996438E + 03 0.2730479755E + 03 0.460530333E + 02 0.2120425083E + 02 0.2120425083E + 01 0.2768741245E + 01 0.3768741245E + 01 0.351240429E + 01 0.3012676665E + 00 0.3012676665E + 00 0.1868346162E + 00 0.1868346162E + 00 0.1868346162E + 00 0.1868346162E + 00 0.1868346162E + 00 0.7766645955E - 01	c_i -0.4772248864E - 02 -0.7551926479E - 02 -0.1151923151E - 01 -0.1688770930E - 01 -0.3300383374E - 01 -0.3412923411E - 01 -0.5692007677E - 01 -0.6976617596E - 01 -0.7872832352E - 01 -0.787363878E - 01 -0.7269482807E - 01 0.133206894E + 00 0.1415043291E + 00 0.9241690290E - 01	α_i 0.2657973404E + 05 0.4875781996E + 04 0.1365729337E + 04 0.4706688272E + 03 0.1846809908E + 03 0.7938436608E + 02 0.3654888101E + 02 0.1776447645E + 02 0.1776447645E + 02 0.9025753924E + 01 0.4760750694E + 01 0.2594749692E + 01 0.1457134036E + 01 0.8418759738E + 00 0.3048852805E + 00 0.1904575230E + 00 0.1904575230E + 00 0.125008409E + 00	$\begin{array}{c} c_i\\ -0.3634920018E-02\\ -0.5752657548E-02\\ -0.8777233728E-02\\ -0.8777233728E-02\\ -0.1287752504E-01\\ -0.1830094211E-01\\ -0.2531192708E-01\\ -0.3412641398E-01\\ -0.3412641398E-01\\ -0.4476266061E-01\\ -0.5671998830E-01\\ -0.6836367592E-01\\ -0.7596024286E-01\\ -0.7275139533E-01\\ -0.7275139533E-01\\ -0.4960311183E-01\\ 0.6942847954E-01\\ 0.1298818803E+00\\ 0.14125027E+00\\ \end{array}$		
α_i 0.1541972558E + 05 0.2828589380E + 04 0.7922996438E + 03 0.2730479755E + 03 0.1071382784E + 03 0.4605330333E + 02 0.2120425083E + 02 0.130836509E + 02 0.5240720981E + 01 0.2768741245E + 01 0.3512676665E + 00 0.3012676665E + 00 0.3012676665E + 00 0.312676665E + 00 0.312676665E + 00 0.312676655E + 00 0.31267665E + 00 0.	c_{i} -0.4772248864E - 02 -0.7551926479E - 02 -0.151923151E - 01 -0.1688770930E - 01 -0.2395701308E - 01 -0.3300383374E - 01 -0.4412923411E - 01 -0.5692007677E - 01 -0.6976617596E - 01 -0.7872832352E - 01 -0.7637363878E - 01 -0.7637363878E - 01 -0.763482807E - 01 0.7269482807E - 01 0.1333206894E + 00 0.1415043291E + 00 0.9241690309E - 01 0.330927624E - 01	α_i 0.2657973404E + 05 0.4875781996E + 04 0.1365729337E + 04 0.4706688272E + 03 0.1846809908E + 03 0.7938436608E + 02 0.3654888101E + 02 0.1776447645E + 02 0.9025753924E + 01 0.4760750694E + 01 0.2594749692E + 01 0.1457134036E + 01 0.8418759738E + 00 0.3048852805E + 00 0.1904575230E + 00 0.1215008409E + 00 0.7988442962E - 01	$\begin{array}{c} -1.2(-14) \\ & c_i \\ -0.3634920018E - 02 \\ -0.5752657548E - 02 \\ -0.577233728E - 02 \\ -0.1287752504E - 01 \\ -0.2531192708E - 01 \\ -0.3412641398E - 01 \\ -0.3412641398E - 01 \\ -0.4476266061E - 01 \\ -0.5671998830E - 01 \\ -0.7596024286E - 01 \\ -0.7596024286E - 01 \\ -0.7596024286E - 01 \\ -0.759533E - 01 \\ -0.4960311183E - 01 \\ 0.6942847954E - 01 \\ 0.1298818803E + 00 \\ 0.1418125027E + 00 \\ 0.958761667E + 01 \\ \end{array}$		
α_i 0.1541972558E + 05 0.2828589380E + 04 0.7922996438E + 03 0.2730479755E + 03 0.1071382784E + 03 0.4605330333E + 02 0.2120425083E + 02 0.120425083E + 02 0.5240720981E + 01 0.5240720981E + 01 0.3562083030E + 00 0.3012676665E + 00 0.1868346162E + 00 0.1187939635E + 00 0.7705045957E - 01 0.5320728144E - 01	c_{i} -0.4772248864E - 02 -0.7551926479E - 02 -0.1151923151E - 01 -0.1688770930E - 01 -0.2395701308E - 01 -0.3300383374E - 01 -0.4412923411E - 01 -0.5692007677E - 01 -0.6976617596E - 01 -0.7872832352E - 01 -0.7637363878E - 01 0.7269482807E - 01 0.7269482807E - 01 0.1333206894E + 00 0.1415043291E + 00 0.9241690309E - 01 0.3320997063E - 01 0.5099261175E - 02	α_i 0.2657973404E + 05 0.4875781996E + 04 0.1365729337E + 04 0.4706688272E + 03 0.1846809908E + 03 0.7938436608E + 02 0.3654888101E + 02 0.1776447645E + 02 0.9025753924E + 01 0.4760750694E + 01 0.4760750694E + 01 0.457134036E + 01 0.8418759738E + 00 0.3048852805E + 00 0.1904575230E + 00 0.1215008409E + 00 0.7883442862E - 01 0.51777378205E = 01	$\begin{array}{c} c_{i} \\ -0.3634920018E - 02 \\ -0.5752657548E - 02 \\ -0.577233728E - 02 \\ -0.1287752504E - 01 \\ -0.1830094211E - 01 \\ -0.2531192708E - 01 \\ -0.3412641398E - 01 \\ -0.4476266061E - 01 \\ -0.5671998830E - 01 \\ -0.5671998830E - 01 \\ -0.7596024286E - 01 \\ -0.7275139533E - 01 \\ -0.4960311183E - 01 \\ 0.6942847954E - 01 \\ 0.6942847954E - 01 \\ 0.1298818803E + 00 \\ 0.1418125027E + 00 \\ 0.9587261667E - 01 \\ -0.3590034614E - 01 \\ \end{array}$		
α_i 0.1541972558E + 05 0.2828589380E + 04 0.7922996438E + 03 0.2730479755E + 03 0.1071382784E + 03 0.4605330333E + 02 0.2120425083E + 02 0.1203836509E + 02 0.5240720981E + 01 0.5240720981E + 01 0.35262833030E + 00 0.3012676665E + 00 0.1868346162E + 00 0.1868346162E + 00 0.1868346162E + 00 0.1868346162E + 00 0.7705045957E - 01 0.5064910346E - 01 0.339278144E - 01 0.2155235940E - 01	c_i -0.4772248864E - 02 -0.7551926479E - 02 -0.7551926479E - 02 -0.1151923151E - 01 -0.1688770930E - 01 -0.3300383374E - 01 -0.3300383374E - 01 -0.4412923411E - 01 -0.5692007677E - 01 -0.5692007677E - 01 -0.7872832352E - 01 -0.7872832352E - 01 -0.7872832352E - 01 -0.7269482807E - 01 0.733206894E + 00 0.1415043291E + 00 0.9241690309E - 01 0.3320997063E - 01 0.508986175E - 02 0.183528065E - 02	α_i 0.2657973404E + 05 0.4875781996E + 04 0.1365729337E + 04 0.4706688272E + 03 0.1846809908E + 03 0.7938436608E + 02 0.3654888101E + 02 0.1776447645E + 02 0.9025753924E + 01 0.4760750694E + 01 0.2594749692E + 01 0.1457134036E + 01 0.8418759738E + 00 0.3048852805E + 00 0.1904575230E + 00 0.1215008409E + 00 0.7883442862E - 01 0.5173782054E - 01 0.340204673E - 01	$\begin{array}{c} c_{1} \\ -0.3634920018E - 02 \\ -0.5752657548E - 02 \\ -0.5752657548E - 02 \\ -0.8777233728E - 02 \\ -0.1287752504E - 01 \\ -0.1830094211E - 01 \\ -0.3412641398E - 01 \\ -0.3412641398E - 01 \\ -0.4476266061E - 01 \\ -0.5671998830E - 01 \\ -0.567024286E - 01 \\ -0.7596024286E - 01 \\ -0.7596024286E - 01 \\ -0.7596024286E - 01 \\ -0.4960311183E - 01 \\ -0.6942847954E - 01 \\ 0.6942847954E - 01 \\ 0.1298818803E + 00 \\ 0.1418125027E + 00 \\ 0.9587261667E - 01 \\ 0.558004614E - 01 \\ 0.5713055804E - 02 \\ \end{array}$		
α_i 0.1541972558E + 05 0.2828589380E + 04 0.7922996438E + 03 0.7922996438E + 03 0.2730479755E + 03 0.1071382784E + 03 0.4605330333E + 02 0.2120425083E + 02 0.1030836509E + 02 0.5240720981E + 01 0.5264741245E + 01 0.3512676655E + 00 0.3012676665E + 00 0.1187939635E + 00 0.7105045957E - 01 0.5064910346E - 01 0.3339778144E - 01 0.2155235949E - 01	c_i -0.4772248864E - 02 -0.7551926479E - 02 -0.1151923151E - 01 -0.1688770930E - 01 -0.3300383374E - 01 -0.3300383374E - 01 -0.4412923411E - 01 -0.6976617596E - 01 -0.6976617596E - 01 -0.787363878E - 01 -0.7269482807E - 01 0.733206894E + 00 0.1415043291E + 00 0.1415043291E + 00 0.9241690309E - 01 0.3320997063E - 01 0.5089861175E - 02 0.1835280626E - 03	α_i 0.2657973404E + 05 0.4875781996E + 04 0.1365729337E + 04 0.4706688272E + 03 0.1846809908E + 03 0.7938436608E + 02 0.3654888101E + 02 0.3654888101E + 02 0.3654888101E + 02 0.1776447645E + 01 0.4760750694E + 01 0.457134036E + 01 0.457134036E + 01 0.3048852805E + 00 0.1904575230E + 00 0.1215008409E + 00 0.7883442862E - 01 0.5173782054E - 01 0.3402046743E - 01 0.3402046743E - 01 0.217792900E - 01	$\begin{array}{c} c_{i} \\ -0.3634920018E - 02 \\ -0.5752657548E - 02 \\ -0.8777233728E - 02 \\ -0.1287752504E - 01 \\ -0.1830094211E - 01 \\ -0.2531192708E - 01 \\ -0.3412641398E - 01 \\ -0.3412641398E - 01 \\ -0.4476266061E - 01 \\ -0.5671998830E - 01 \\ -0.6836367592E - 01 \\ -0.7596024286E - 01 \\ -0.7275139533E - 01 \\ -0.4960311183E - 01 \\ -0.6942847954E - 01 \\ 0.1298818803E + 00 \\ 0.1418125027E + 00 \\ 0.9587261667E - 01 \\ 0.3580034614E - 01 \\ 0.5713055894E - 02 \\ 0.2148358286E - 03 \\ \end{array}$		
α_i 0.1541972558E + 05 0.2828589380E + 04 0.7922996438E + 03 0.7922996438E + 03 0.2730479755E + 03 0.1071382784E + 03 0.4605330333E + 02 0.2120425083E + 02 0.2120425083E + 01 0.2768741245E + 01 0.2768741245E + 01 0.3012676665E + 00 0.3012676665E + 00 0.3012676665E + 00 0.1868346162E + 00 0.3187393635E + 00 0.7705049557E - 01 0.5064910346E - 01 0.3339778144E - 01 0.2155235949E - 01	c_i -0.4772248864E - 02 -0.7551926479E - 02 -0.1151923151E - 01 -0.1688770930E - 01 -0.3300383374E - 01 -0.3300383374E - 01 -0.4412923411E - 01 -0.569200767E - 01 -0.6976617596E - 01 -0.7872832352E - 01 -0.7637363878E - 01 -0.7269482807E - 01 0.7269482807E - 01 0.133206894E + 00 0.1415043291E + 00 0.1415043291E + 00 0.320997063E - 01 0.5089861175E - 02 0.1835280626E - 03	α_i 0.2657973404E + 05 0.4875781996E + 04 0.1365729337E + 04 0.4706688272E + 03 0.1846809908E + 03 0.7938436608E + 02 0.3654888101E + 02 0.3654888101E + 02 0.1776447645E + 02 0.9025753924E + 01 0.4760750694E + 01 0.2594749692E + 01 0.1457134036E + 01 0.3048852805E + 00 0.1904575230E + 00 0.1904575230E + 00 0.1215008409E + 00 0.5173782054E - 01 0.3402046743E - 01 0.2187792900E - 01	$\begin{array}{c} c_i \\ \hline c_i \\ c_i \\ \hline c_i \\ c_i \\ c_i \\ \hline c_i \\ c$		

TABLE IV (cont.) α - and c-parameters for the STO-NG expansions of the STO-2S with exponent equal to one. (N = 21 to 24).					
STO-21G	STO-21G $\epsilon^{a} = 4.1(-15)$		= 1.9(-15)		
α,	C _t	α	C,		
$\begin{array}{c} 0.4530072752E+05\\ 0.8309962189E+04\\ 0.2327661810E+04\\ 0.8021794061E+03\\ 0.3147598267E+03\\ 0.3147598267E+03\\ 0.352981503E+03\\ 0.6229074524E+02\\ 0.3027388201E+02\\ 0.3027388201E+02\\ 0.3027388201E+02\\ 0.4409817231E+01\\ 0.2467189808E+01\\ 0.4409817231E+01\\ 0.2467189808E+01\\ 0.3071417331E+00\\ 0.3071417331E+00\\ 0.3071417331E+00\\ 0.3071447331E+00\\ 0.1925665380E+00\\ 0.1229739754E+00\\ 0.7974862391E-01\\ 0.5226832576E-01\\ 0.3431180630E-01\\ 0.202532892E-01\\ \end{array}$	$\begin{array}{c} -0.2784342094E-02\\ -0.4406751036E-02\\ -0.6724779756E-02\\ -0.9870508007E-02\\ -0.9870508007E-02\\ -0.1940483475E-01\\ -0.1946483775E-01\\ -0.2636614455E-01\\ -0.2636614455E-01\\ -0.3490886706E-01\\ -0.4504824154E-01\\ -0.5623477746E-01\\ -0.6686873938E-01\\ -0.7346621210E-01\\ -0.6984025114E-01\\ -0.6752651092E-01\\ 0.1281190938E+00\\ 0.1421574469E+00\\ 0.9773989679E-01\\ 0.3712275303E-01\\ -0.6024724761E-02\\ -0.204291059E-03\\ \end{array}$	0.7673959300E + 05 0.1407710962E + 05 0.3943071084E + 04 0.1358897638E + 04 0.533206288E + 03 0.2291966293E + 03 0.1055206421E + 03 0.5128236820E + 02 0.2604575491E + 02 0.7460036820E + 01 0.4165340589E + 01 0.2380503968E + 01 0.1388791323E + 01 0.383529534E + 00 0.3083529534E + 00 0.1936334225E + 00 0.1236842188E + 00 0.8017362133E - 01 0.5250850441E - 01 0.3444122419E - 01	$\begin{array}{c} -0.2139283532E-02\\ -0.3385924081E-02\\ -0.5167466923E-02\\ -0.5167466923E-02\\ -0.7586608010E-02\\ -0.1079914394E-01\\ -0.1498929518E-01\\ -0.2035865178E-01\\ -0.2035865178E-01\\ -0.2353539949E-01\\ -0.4498283951E-01\\ -0.5549147701E-01\\ -0.6535872469E-01\\ -0.6535872469E-01\\ -0.655959731E-01\\ 0.6655959731E-01\\ 0.6655959731E-01\\ 0.1273146780E+00\\ 0.1423828350E+00\\ 0.9863494141E-01\\ 0.3773508648E-01\\ 0.667401012E-02\\ \end{array}$		
		0.2208989827E - 01	0.2375531112E - 03		
STO-23G	$\varepsilon^{\mathbf{a}} = 1.3(-15)$	STO-24G ε ^a	= 3.1(-16)		
STO-23G α _i	$\varepsilon^{a} = 1.3(-15)$ c _i	STO-24G ε ^a : α _i	= 3.1(-16) c _i		
$\begin{array}{c} \textbf{STO-23G} \\ \textbf{\alpha}_i \\ 0.1297556734E + 06 \\ 0.2380238268E + 05 \\ 0.6667172826E + 04 \\ 0.2297704393E + 04 \\ 0.9015776188E + 03 \\ 0.3873398766E + 03 \\ 0.3873398766E + 02 \\ 0.403615311E + 02 \\ 0.2319839528E + 02 \\ 0.2319839528E + 02 \\ 0.2319839528E + 02 \\ 0.2319839528E + 01 \\ 0.2327491928E + 01 \\ 0.307357123E + 01 \\ 0.3227491928E + 01 \\ 0.3089203227E + 00 \\ 0.1260427560E + 02 \\ 0.3089203227E + 00 \\ 0.1941116055E + 00 \\ 0.1239927148E + 00 \\ 0.8035432034E - 01 \\ 0.5260918111E - 01 \\ 0.3449495996E - 01 \\ 0.2211653189E - 01 \\ \end{array}$	c_i -0.1645192157E - 02 -0.2603952874E - 02 -0.3974273114E - 02 -0.3974273114E - 02 -0.3835660488E - 02 -0.8309685381E - 02 -0.1154272946E - 01 -0.1570232573E - 01 -0.296756304E - 01 -0.2750460932E - 01 -0.3541162156E - 01 -0.4460371126E - 01 -0.4460371126E - 01 -0.637829919E - 01 -0.6978139498E - 01 -0.663234367E - 01 -0.6612389856E - 01 0.1269802049E + 00 0.1424975425E + 00 0.9902242192E - 01 0.3799460403E - 01 0.6227436032E - 02 0.2405452167E - 03	$\begin{array}{c} \mathbf{STO-24G} \ \epsilon^{a} \\ \mathbf{a}_{1} \\ \hline \\ \mathbf{a}_{1} \\ \hline \\ \mathbf{0.1196765641E} + 06 \\ \mathbf{0.2195347033E} + 05 \\ \mathbf{0.6149282624E} + 04 \\ \mathbf{0.2119224360E} + 04 \\ \mathbf{0.815459436E} + 03 \\ \mathbf{0.3574383806E} + 03 \\ \mathbf{0.3574383806E} + 03 \\ \mathbf{0.1645643132E} + 03 \\ \mathbf{0.7997990517E} + 02 \\ \mathbf{0.4062462817E} + 02 \\ \mathbf{0.2141027331E} + 02 \\ \mathbf{0.2141027331E} + 02 \\ \mathbf{0.1164512120E} + 02 \\ \mathbf{0.6510310689E} + 01 \\ \mathbf{0.3730039921E} + 01 \\ \mathbf{0.130822983E} + 01 \\ \mathbf{0.8004589519E} + 00 \\ \mathbf{0.3188566460E} + 00 \\ \mathbf{0.2073513908E} + 00 \\ \mathbf{0.3188566460E} + 00 \\ \mathbf{0.9218070796E} - 01 \\ \mathbf{0.6263455177E} - 01 \\ \mathbf{0.4284009934E} - 01 \\ \mathbf{0.2923889886E} - 01 \\ \mathbf{0.1946489210E} - 01 \\ \end{array}$	c_i		

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Gaussian	Expansion	of STO's	

.o 27).	¹ = 2.1(-17)	່ວ	0.8413498275E - 03 -0.1331684185E - 02 -0.2985061859E - 02 -0.2985061859E - 02 -0.2985061859E - 02 -0.5911259161E - 02 -0.8054695890E - 02 -0.1078996138E - 01 -0.185296711E - 01 -0.185296711E - 01 -0.1373051957E - 01 -0.3779023957E - 01 -0.377902398E - 01 -0.5378600795E - 01 -0.5378600795E - 01 -0.5378600795E - 01 -0.5378600795E - 01 -0.5378600795E - 01 -0.5378600795E - 01 -0.53786150659E - 01 -0.579152981E - 01 -0.5779023981E - 01 -0.57915298291E - 01 -0.577922929201 = 01 -0.57915298291E - 01 -0.579152083031E - 01 -0.59132083031E - 01 -0.775567508E - 01 -0.775567508E - 01 -0.775567508E - 01 -0.775567508E - 01	
It equal to one. $(N = 25 t)$	STO-27G ε^3	α	0.4961466479E + 06 0.9101316615E + 05 0.2549327893E + 05 0.344737532E + 04 0.344737532E + 04 0.344737532E + 04 0.3481851281E + 03 0.3315777736E + 03 0.3315777736E + 03 0.6822449416E + 03 0.68225493616E + 03 0.68279334E + 02 0.5875460574E + 02 0.5875460574E + 02 0.5365612923E + 01 0.2546517492E + 01 0.5365612923E + 01 0.3246371489E + 01 0.1294413777E + 01 0.1294427124E + 01 0.120998574E + 00 0.3235225600E + 00 0.3265612923E + 01 0.3265612923E + 01 0.376671293852E + 01 0.3265612923E + 01 0.3765612923E + 01 0.3765612923E + 01 0.3765612923E + 01 0.3765612923E + 01 0.377567447E - 01 0.977267447E - 01 0.977267447E - 01 0.977267447E - 01 0.977267447E - 01 0.977267447E - 01	
E IV (cont.) the STO-2S with exponer	$^{a} = 4.0(-17)$.c.	-0.1063965867E - 02 -0.1684033006E - 02 -0.2570368810E - 02 -0.3774702811E - 02 -0.3776530001E - 02 -0.7473091855E - 01 -0.1017923646E - 01 -0.13712939956E - 01 -0.13712939956E - 01 -0.13712939951E - 01 -0.3740629951E - 01 -0.3740629551E - 01 -0.3740629551E - 01 -0.3740629551E - 01 -0.540363374E - 01 -0.540363374E - 01 -0.541375951E - 01 -0.541375951E - 01 -0.541375951E - 01 -0.5910543434E - 01 -0.5910543434E - 01 -0.5910543434E - 01 -0.510354244E - 01 -0.510354344E - 01 -0.510354344E - 01 -0.5103543434E - 01 -0.510354345E - 01 -0.51034335E + 00 -0.51034335E - 01 -0.510366014783E - 01 -0.751516265E - 01 -0.710975512E - 04	
TABLE STO-NG expansions of t	ST0-26G E	α	0.3102466583E + 06 0.5691166037E + 05 0.1594126173E + 05 0.1594126173E + 04 0.2155685367E + 04 0.22155685367E + 04 0.20739303244E + 03 0.2073392008E + 03 0.2073392008E + 03 0.3018097459E + 02 0.3018097459E + 02 0.3018097459E + 02 0.3641484726E + 01 0.3641484726E + 01 0.3661226764E + 01 0.3561256764E + 01 0.3561256764E + 01 0.3561256764E + 01 0.3361256764E + 01 0.20380415577E + 01 0.3361256771E + 01 0.3361256771E + 01 0.3361256771E + 01 0.3361256771E + 01 0.3361256771E + 01 0.2038015771E + 01 0.205997371E + 01	
nd c-parameters for the	a = 1.0(-16)	ບ້	-0.1347824918E - 02 -0.2133308162E - 02 -0.2133308162E - 02 -0.4781383645E - 02 -0.6809537624E - 02 -0.6809537624E - 02 -0.1288132501E - 01 -0.1722412208E - 01 -0.17265026546E - 01 -0.2265026546E - 01 -0.2265026546E - 01 -0.3716753834E - 01 -0.460713501E - 01 -0.460713501E - 01 -0.602283635056E - 01 -0.60217877640E - 01 -0.60217877640E - 01 -0.60217877640E - 01 -0.60217877640E - 01 -0.601807782016 - 01 -0.601807765408E - 01 -0.6018077660E - 01 -0.6022836360E - 01 -0.6022836360E - 01 -0.575360109E - 02 0.5753360109E - 02 0.5753360109E - 02 0.5753360109E - 02	m of the expansion.
α- a	STO-25G 5 ⁴	້ອ	$\begin{array}{c} 0.1933277897E + 06\\ 0.3546405578E + 05\\ 0.3546405578E + 04\\ 0.3423437914E + 04\\ 0.3423437914E + 04\\ 0.1343297213E + 04\\ 0.1343297213E + 02\\ 0.5774143337E + 03\\ 0.2558413439E + 03\\ 0.2558413439E + 02\\ 0.1880843302E + 02\\ 0.1880843302E + 02\\ 0.1051153157E + 02\\ 0.1393683321E + 01\\ 0.2954872414E - 01\\ 0.295487243E - 01\\ 0.1962960068E - 01\\ $	suuared error in the norr
				Š

	Three-cen	TABLE V ter nuclear attraction integrals.	
N	Integral I	Integral II	Integral III
13 14 15	0.0075741015 0.0075742296 0.0075742268	0.04116619724 0.04116638702 0.04116645735	0.07173271572 0.07173283686 0.07173288410
16 17 18 19	0.0075742644 0.0075742647 0.0075742761 0.0075742768	0.04116649508 0.04116651127 0.04116651828 0.04116652325	0.07173292406 0.07173294232 0.07173294893 0.07173295327
20 21 22	0.0075742802 0.0075742809 0.0075742818 0.0075742818	0.04116652611 0.04116652750 0.04116652837 0.04116652886	0.07173295525 0.07173295599 0.07173295669 0.07173295715
23 24 25 26	0.0075742822 0.0075742824 0.0075742827 0.0075742827	0.04116652905 0.04116652914 0.04116652920	0.07173295732 0.07173295732 0.07173295739 0.07173295745
27 Other authors' ¹⁵	0.0075742828	0.04116652923	0.07173295748 0.071732965
All integrals a	re of the form $< 1s^{A}$	$r_{C}^{-1} 1s^{B} >$	
Integral	I A: $(0, 0, 0)$ B: $(2, 0, 0)$ C: $(1, 1.73205, 0)$ $\zeta^{A} = 0.2$ $\zeta^{B} = 10.0$)	
Integral	II A: $(0, 0, 0)$ B: $(2, 0, 0)$ C: $(-0.5, 0, 0)$ $\zeta^{A} = 1.0$ $\zeta^{B} = 5.0$		
Integral	III A: $(0, 0, 0)$ B: $(2, 0, 0)$ C: $(0.5, 0, 0)$ $\zeta^{A} = 1.0$ $\zeta^{B} = 5.0$		

TABLE VI								
Many-center electron repulsion integrals.								
N	Inte	egral I	Integral II	Integral III	Integral IV			
13 14 15 16 17 18 19 20 21 22 23 24 25 26 27	0.19446 0.19446 0.19446 0.19446 0.19446 0.19446 0.19446 0.19446 0.19446 0.19446 0.19446 0.19446 0.19446 0.19446	88677192 88666269 88680287 88676775 88676478 88676478 88676386 88676033 88676138 88676161 88676170 88676177 88676172	0.000128167676 0.000128156646 0.000128156025 0.000128159857 0.000128162562 0.000128162562 0.000128162871 0.000128162650 0.000128162650 0.000128162959 0.000128162959 0.000128162976 0.000128162968 0.000128162976	0.3455378141237 0.3455378154938 0.3455378154938 0.3455378150222 0.3455378150930 0.3455378150506 0.3455378150489 0.3455378150489 0.3455378150441 0.34553781504452 0.3455378150440 0.3455378150444 0.3455378150444	0.0021169819938 0.0021169834517 0.0021169831262 0.0021169827234 0.0021169827699 0.0021169827699 0.0021169827893 0.0021169827843 0.0021169827843 0.0021169827849 0.0021169827870 0.0021169827869 0.0021169827869			
Other authors ^{, 16}	0.01944	69.	0.0001281719	0.3455	0.0021			
Integral I A: (0, 0 B: (2, 0, C: (0, 0 D: (1, 1		A: (0, 0, 0) B: (2, 0, 0) C: (0, 0, 0) D: (1, 1, 0)	1s ^A (1.2) 1s ^B (1.2) 1s ^C (1.2) 1s ^D (1.2)					
Integral II A: (0, B: (0, C: (0, D: (0		A: (0, 0, 0) B: (0, 7.5, 0 C: (0, 2.5, 0 D: (0, 2.5, 0	$1s^{A} (5.7)$ $1s^{B} (1.0)$ $2s^{C} (2.6)$ $1s^{D} (1.0)$					
Integral III		A: (0, 0, 0) B: (1, 0, 0) C: (0, 1, 0) D: (0, 0, 1)	1s ^A (1.0) 1s ^B (1.0) 1s ^C (1.0) 1s ^D (1.0)					
Integral IV		A: (0, 0, 0) B: (1, 0, 0) C: (0, 1, 0) D: (1, 1, 0)	1s ^A (6.0) 1s ^B (6.0) 1s ^C (6.0) 1s ^D (6.0)					

TABLE VII Many-center electron repulsion integrals with high quantum numbers.								
N	Integral I	Integral II	Integral III	Integral IV				
13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 11 11 11 11 11 11	$\begin{array}{c} -0.0141752422071\\ -0.0141752422033\\ -0.0141752424622\\ -0.0141752424632\\ -0.0141752424959\\ -0.0141752424810\\ -0.0141752425074\\ -0.0141752425074\\ -0.0141752425034\\ -0.0141752425034\\ -0.0141752425038\\ -0.0141752425049\\ -0.0141752425046\\ -0.0141752425046\\ -0.0141752425046\\ \end{array}$	$\begin{array}{c} 0.0152948544673\\ 0.0152948553564\\ 0.0152948556922\\ 0.0152948556922\\ 0.015294855692\\ 0.0152948555471\\ 0.0152948555080\\ 0.0152948555080\\ 0.0152948555162\\ 0.0152948555162\\ 0.0152948555183\\ 0.0152948555183\\ 0.0152948555183\\ 0.0152948555183\\ 0.0152948555183\\ 0.0152948555183\\ 0.0152948555183\\ 0.0152948555183\\ 0.0152948555183\\ 0.0152948555183\\ 0.0152948555183\\ 0.0152948555183\\ 0.0152948555183\\ 0.0152948555183\\ 0.0152948555183\\ 0.0152948555183\\ 0.0152948555183\\ 0.0152948555183\\ 0.0152948555183\\ 0.015294855183\\ 0.0152948555183\\ 0.0152948555183\\ 0.0152948555183\\ 0.0152948555183\\ 0.0152948555183\\ 0.0152948555183\\ 0.0152948555183\\ 0.0152948555183\\ 0.0152948555183\\ 0.0152948555183\\ 0.0152948555183\\ 0.0152948555183\\ 0.0152948555183\\ 0.0152948555183\\ 0.0152948555183\\ 0.0152948555183\\ 0.015294855682\\ 0.015294855682\\ 0.015294855682\\ 0.015294855682\\ 0.015294855682\\ 0.015294855682\\ 0.015294855682\\ 0.015294855682\\ 0.015294855682\\ 0.015294855682\\ 0.015294855682\\ 0.015294855682\\ 0.015294855682\\ 0.015294855882\\ 0.015294855882\\ 0.015294855682\\ 0.015294855882\\ 0.015294855682\\ 0.015294855882\\ 0.015294855682\\ 0.015294855682\\ 0.015294855682\\ 0.015294855682\\ 0.015294855882\\ 0.015294855882\\ 0.015294855882\\ 0.015294855882\\ 0.015294855882\\ 0.015294855882\\ 0.015294855882\\ 0.015294855882\\ 0.015294855882\\ 0.015294855882\\ 0.015294855882\\ 0.01529485582\\ 0.01529485582\\ 0.015294855882\\ 0.015294855882\\ 0.015294855882\\ 0.015294855882\\ 0.015294855882\\ 0.015294855882\\ 0.015294855882\\ 0.015294855882\\ 0.015294855882\\ 0.015294855882\\ 0.01529485582\\ 0.01529485582\\ 0.01529485582\\ 0.01529485582\\ 0.01529485582\\ 0.01529485582\\ 0.01529485582\\ 0.01529485582\\ 0.01529485582\\ 0.01529485582\\ 0.01529485582\\ 0.01529485582\\ 0.01529485582\\ 0.01529485582\\ 0.01529485582\\ 0.01529485582\\ 0.01529485582\\ 0.01529485582\\ 0.0152948582\\ 0.01529485582\\ 0.01529485582\\ 0.01529485582\\ 0.01529485582\\ 0.01529485582\\ 0.01529485582\\ 0.01529485582\\ 0.01529485582\\ 0.01529485582\\ 0.0152948558\\ 0.0152948558\\ 0.01529485582\\ 0.0152948558\\ 0.015294858\\ 0.016282\\ 0.0152948558\\ 0.0152948558$	0.0245956549957 0.0245956564199 0.02459565670091 0.0245956567031 0.0245956567262 0.0245956567262 0.0245956567688 0.0245956567459 0.02459565674459 0.0245956567492 0.0245956567492 0.0245956567487 0.0245956567483	-0.0070857513990 -0.0070857443050 -0.007085731709 -0.0070857393590 -0.0070857393254 -0.0070857392250 -0.0070857392156 -0.0070857392192 -0.0070857392192 -0.0070857392196 -0.0070857392167 -0.0070857392169 -0.0070857392171				
All the exponents equal to 1.56788.								

many-center integrals as those reported in the previous work¹. As no other results of higher accuracy were available in the literature, the accuracy was estimated by testing the convergence of the integral values as the expansions were extended. The results obtained in the selected three-center nuclear attraction integrals are presented in Table V.

An interesting feature of these results (confirmed by other calculations that we have carried out with this aim) is that the absolute error remains almost constant for a given expansion, independently of the exponents of the STO's and distances between the centers. For instance, in case of the STO-27G expansion, this error is about 10^{-10} .

In Tables VI and VII the corresponding results for some three- and four-center electron repulsion integrals are collected. For a given expansion, the accuracy achieved in these integrals is higher than that obtained in the three-center nuclear attraction integrals. An absolute error of about 10^{-12} is attained with the STO-27G

expansion, while the STO-12G yields, for the same case, only four correct figures and an absolute error of about 10^{-8} .*

As it was previously suggested, the fact that better results are obtained for electron repulsion integrals than for three-center nuclear attraction integrals may be explained by the different nature of the two types of integrals: the former depend on the potential throughout the whole space, whereas the latter depend on point values of the potential.

The above results clearly show that the STO-27G expansion provides a means accurate enough for testing other algorithms and procedures designed for the calculation of many-center molecular integrals with Slater basis functions.

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* It should be noticed that there is a misprint in some of our previously reported results (Table VI of ref.¹) where the integral values are incorrectly multiplied by a factor of 10.